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#### **Report Title**

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# Low-temperature spin spray deposited ferrite/piezoelectric thin film magnetoelectric heterostructures with strong magnetoelectric coupling

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**Abstract** We report low-temperature spin spray deposited Fe<sub>3</sub>O<sub>4</sub>/ZnO thin film microwave magnetic/piezoelectric magnetoelectric heterostructures. A voltage induced effective ferromagnetic resonance field of 14 Oe was realized in Fe<sub>3</sub>O<sub>4</sub>/ZnO magnetoelectric (ME) heterostructures. Compared with most thin film magnetoelectric heterostructures prepared by high temperature (>600 °C) deposition methods, for example, pulsed laser deposition, molecular beam epitaxy, or sputtering, Fe<sub>3</sub>O<sub>4</sub>/ZnO ME heterostructures have much lower deposition temperature (<100 °C) at a much lower cost and less energy dissipation, which can be readily integrated in different integrated circuits.

#### 1 Introduction

Layered magnetoelectric (ME) heterostructures with two or more constituent phases of ferro/ferrimagnetic and piezo/ ferroelectric phases have gained a lot of recent interest due

Z. Zhou and O. Obi have contributed equally to this work.

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K. Mahalingam · M. Liu · G. J. Brown Materials and Manufacturing Directorate, Air Force Research Laboratory, Wright Patterson, AFB, OH 45433 7707, USA to the strong strain mediated ME coupling between the ferro/ferrimagnetic and piezo/ferroelectric phases in ME heterostructures. Magnetoelectric heterostructure enables electric field control of magnetism or vice versa [1 6]. The ME coupling in multiferroics has led to different ME devices, such as picotesla magnetic sensors [7], electric field tunable RF/microwave magnetic devices [8 11], tunable resonators [8], phase shifters [9], tunable inductors [10] and tunable filters [11]. Compared to state of the art microwave magnetic devices tuned by magnetic fields, the electric field or voltage tunable ME devices are much more energy efficient, lightweight, compact, and less noisy.

Studies on ME heterostructures are mostly based on complex oxide piezoelectric ceramic or single crystal, such as lead zirconate titanate, barium titanate, lead zinc niobate lead titanate (PZN-PT), lead magnesium niobatelead titanate, etc. Most of these thin film ME heterostructures are typically grown by pulsed laser deposition [12], molecular beam epitaxy [13], chemical solution deposition [14], sputtering [5, 6] or pyrolyzing [15]. These deposition methods for ME heterostructures require high processing temperatures of >600 °C, which leads to interface diffusion and degraded RF magnetism or piezoelectricity [14]. The high process temperatures make it very challenging in integrating these ME devices onto radio frequency integrated circuits or monolithic microwave integrated circuits.

Spin-spray deposition method is a unique wet chemical technique for synthesizing high crystalline quality, low-loss and fully dense RF/microwave complex oxide films. For example, spinel ferrites thin film can be fabricated directly from aqueous solution at  $\sim 90$  °C through this method. The processing temperature is much lower than that of (>600 °C) other ferrite preparation methods [16 18]. In addition, tight atomic bonding can be formed at the interface between spin-spray synthesized ferrite films and



ferroelectrics, with minimal interface inter-diffusion, which leads to strong ME coupling and thereby provides great opportunities for ME heterostructures. Using this method, a giant electric field induced effective magnetic field of 860 Oe has been demonstrated in a Fe<sub>3</sub>O<sub>4</sub>/PZN-PT magnetic thin film/piezoelectric slab heterostructures [16]. Although spin spray deposition of ferrite films has been widely performed [16], the spin spray deposition of ferroelectrics or piezoelectrics is rarely explored, except for a recent demonstration of a spin spray deposited ZnO films [17, 18]. ZnO is a typical piezoelectric material, which makes it a good candidate for thin film ME heterostructures at low temperatures. ZnO is also a direct wide band gap semiconductor with excellent electrical and optical properties which makes it applicable in a wide variety of electron, optoelectronic, spintronics and nanodevices [17, 18]. The piezoelectric properties of spin spray deposited ZnO films when combined with spin spray deposited ferrites offer a unique opportunity for low-temperature synthesized ferrite/ZnO ME heterostructures, and novel integrated voltage tunable RF/microwave ME devices.

In this communication, we demonstrate ME ferrite/piezoelectric thin film heterostructures of Fe<sub>3</sub>O<sub>4</sub> (1.4 μm)/ ZnO (3 µm) fabricated by the spin-spray process on a glass substrate. A clean interface with negligible inter-diffusion between Fe<sub>3</sub>O<sub>4</sub> and ZnO layers was obtained from the lowtemperature deposition, which led to a tight interface bonding and strong ME coupling. This is in sharp contrast to other ME heterostructures deposited by other hightemperature deposition methods above [5, 6, 12 15]. Strong static and microwave ME interactions were observed in the Fe<sub>3</sub>O<sub>4</sub>/ZnO ME heterostructure. A large voltage induced effective magnetic field of 14 Oe was observed through voltage induced in-plane ferromagnetic resonance (FMR) field shift in the Fe<sub>3</sub>O<sub>4</sub>/ZnO heterostructures. Compared to the high process temperature of >600 °C involved in the deposition process of these thin film heterostructures [12, 13], this low temperature spinspray processing fabricated ME heterostructures provide a viable route to integration of complex oxide thin film ME structures on integrated circuits.

#### 2 Experiment

Fe<sub>3</sub>O<sub>4</sub> (1.4  $\mu$ m)/ZnO (3  $\mu$ m) magnetoelectric ferrite/piezoelectric thin film heterostructures fabricated by the spin-spray process on a glass substrate (0.2 mm). The Fe<sub>3</sub>O<sub>4</sub>/ZnO heterostructure composition was confirmed by X-ray diffraction (XRD) patterns using conventional Bragg Brentano diffraction geometry. The cross-section of Fe<sub>3</sub>O<sub>4</sub>/ZnO structure was determined by energy-filtered transmission electron microscope (EFTEM) imaging. The

crystallographic texture of the thin film Fe $_3O_4$  (1.4 µm)/ZnO (3 µm) heterostructure was further investigated via XRD at beam-line 11-ID-C of the Advanced Photon Source [19 21] using an X-ray wavelength of  $\lambda=0.10804$  Å. Static ME coupling of thin films Fe $_3O_4$ /ZnO ME heterostructures was investigated by electric-field induced changes in a vibrating sample magnetometer (VSM). Piezoelectric coefficient of ZnO film was obtained by a photonic sensor. Microwave ME coupling of thin films Fe $_3O_4$ /ZnO heterostructures was carried out by custommade microwave FMR spectrometer.

#### 3 Results and discussion

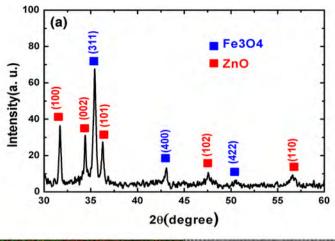
## 3.1 Characterization of Fe<sub>3</sub>O<sub>4</sub>/ZnO thin films heterostructure

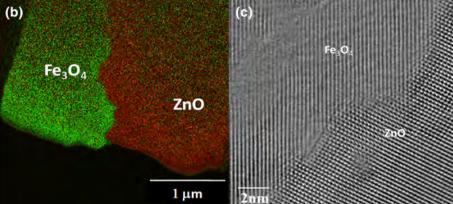
Figure 1a shows the XRD patterns of Fe<sub>3</sub>O<sub>4</sub>/ZnO heterostructure. A clear polycrystalline spinel ferrite phase and a typical ZnO wurtzite structure with no strong preferred orientation is apparent in the Fe<sub>3</sub>O<sub>4</sub> and ZnO films. Figure 1b is an EFTEM image showing the ZnO/Fe<sub>3</sub>O<sub>4</sub> structure in cross-section. The EFTEM imaging was performed based on the three-window technique [22]. This is a composite (RGB) image constructed by superimposing two independent maps of Fe (green) and Zn (red) distribution across the whole structure. A sharp boundary distinguishing the two layers is evident, indicating insignificant interdiffusion at the interface. This is also supported by further examination of this region by high-resolution transmission electron microscopy, shown in Fig. 1c, which reveals the presence of an abrupt and well defined interface between the ZnO and Fe<sub>3</sub>O<sub>4</sub> layers.

The crystallographic texture of the thin film Fe<sub>3</sub>O<sub>4</sub> (1.4 µm)/ZnO (3 µm) heterostructure was further investigated via XRD at beam-line 11-ID-C of the Advanced Photon Source [19 21] using an X-ray wavelength of  $\lambda = 0.10804$  Å. The measured diffraction image is shown in Fig. 2a and a  $2\theta$  section is extracted from  $2.1^{\circ}$  to  $6.2^{\circ}$ over the azimuthal angle from 0° to 180° and shown in Fig. 2b. The positions of the ZnO, Fe<sub>3</sub>O<sub>4</sub> and copper diffraction intensities are also indicated at the top of Fig. 2b for complete phase identification. The ZnO (10.0) diffraction intensities are observed at the lowest  $2\theta$  position (corresponding to an inter-planar distance, or d, of 2.81 Å) and the ZnO (00.2) diffraction intensities are observed at the next highest  $2\theta$  position (d = 2.603 Å). Both ZnO (10.0) and (00.2) are non-uniform with azimuthal angle, with the (10.0) intensity being concentrated around azimuthal angles of 0° and 180° (parallel to the plane of the film) and the (00.2) intensity being concentrated around an azimuthal angle of 90° (in the direction normal to the film).



Fig. 1 a X ray diffraction pattern of the spin spray deposited Fe3O4/ZnO thin films ME composite; **b** Energy Filtered TEM image showing the zinc oxide (*red*) and iron oxide (*green*) layers; **c** HRTEM image of the iron oxide/zinc oxide interface (Color figure online)





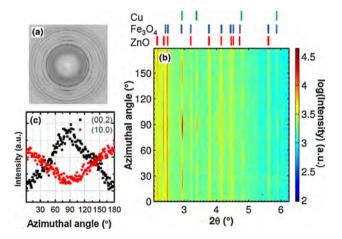


Fig. 2 a The measured X ray diffraction image using high energy X rays in transmission geometry;  $\mathbf{b}$  a  $2\theta$  section from  $2.1^\circ$  to  $6.2^\circ$  over the azimuthal angle from  $0^\circ$  to  $180^\circ$ ;  $\mathbf{c}$  the distribution of the ZnO (10.0) and (00.2) diffraction intensities over the azimuthal angle of the detector were extracted and are presented

The distribution of the ZnO (10.0) and (00.2) diffraction intensities over the azimuthal angle of the detector were extracted and are presented in Fig. 2c. These intensity distributions indicate that the ZnO film is 00.h-type fiber textured. To quantify the strength of the ZnO (00.h)

texture, peak fitting was performed on the (00.h) peak using the curve fitting toolbox in MATLAB© (version R2011b) and the full width at half maximum of this diffraction peak is determined to be  $76^{\circ} \pm 4.8^{\circ}$ .

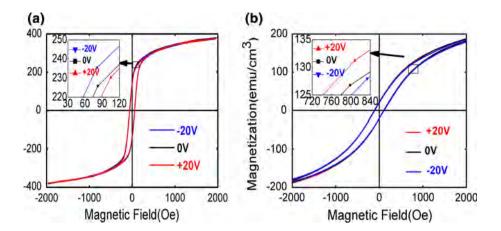
## 3.2 Static ME coupling measurements of Fe<sub>3</sub>O<sub>4</sub>/ZnO heterostructure

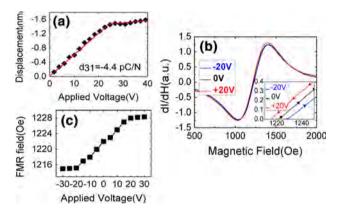
Static ME coupling of thin films  $Fe_3O_4/ZnO$  ME heterostructures was investigated by electric-field induced changes in a VSM for magnetic hysteresis loops measurements as shown in Fig. 3a, b. This was done by applying an external electric-field (E-field) perpendicular to the ZnO film plane (that is, through the thickness direction). The E-field applied to the ZnO thin film led to strain/stress in the  $Fe_3O_4/ZnO$  heterostructure. Magnetization changes were created by the electric-field induced strain due to the inverse magneto-elastic effect. Therefore, electric-field tuning of magnetization can be realized in the ME heterostructure composites through the strain/stress mediated ME coupling.

Figure 3a shows the magnetic hysteresis under different voltages from -20 to 20 V, corresponding to  $\pm$  67 kV/cm electric field (E-field), applied across the thickness



Fig. 3 a In plane magnetic hysteresis loops of the Fe3O4/ZnO ME heterostructure under different electric voltages.
b Out of plane magnetic hysteresis loops of the Fe3O4/ZnO ME heterostructure. The enlarged ME coupling hysteresis loop shift is shown on upper left inset on both figures





**Fig. 4** a Piezoelectric coefficient measurements of ZnO thin film; **b** electric field dependence of the in plane field sweep FMR spectra of the Fe3O4/ZnO ME heterostructure measured at 9.3 GHz. The zero cross part was enlarged to demonstrate a clear ME coupling shift at *bottom right inset*; **c** X band in plane ferromagnetic resonance (FMR) field of the Fe3O4/ZnO heterostructure measured at varying applied voltages across the ZnO layer

direction of the ZnO layer, which is about  $\Delta M/M = 6.5 \%$  under a constant bias field of 100 Oe. The electric field induced magnetization change is small due to the substrate clamping effect, thin thickness of the ZnO (3.0 µm) and small piezoelectric coefficient of ZnO,  $d_{33} = 10.1$  pC/N,  $d_{31} = -5.0$  pC/N, [18] which lead to a relatively small ME coupling coefficient. Figure 3b demonstrated out-of-plane magnetic hysteresis under different electric field induced ME coupling, which indicated  $\Delta M/M = 1.9 \%$  at a bias field of 840 Oe.

Piezoelectric coefficient of ZnO film was obtained by measuring the substrate bending effect [23]. Upon applying an electric field, substrate bending can be anticipated in ZnO/ glass heterostructure. Assuming one side of the specimen is fixed, the bending displacement  $\delta$  can be calculated as [23]:

$$\delta = \frac{1}{2}\kappa L^2 = \frac{L^2}{2t_p} \frac{6AB(1+B)}{A^2B^4 + 2A(2B+3B^2+2B^3) + 1} \cdot d_{31}E_3$$
(1)

where  $\kappa$  is curvature,  $A = Y_S/Y_P$ ,  $B = t_S/t_P$ ,  $Y_S$  is the Young's modulus of the glass substrate layer ( $Y_S = 48$  GPa),  $Y_P$  is the Young's modulus of ZnO piezoelectric layer ( $Y_P = 17$  GPa), tS the thickness of the glass substrate layer ( $t_S = 0.2$  mm) and tP the thickness of the piezoelectric layer (Electric field  $E_3$  was applied along ZnO thickness direction. The sample was cut into length L = 2 cm, width of 0.5 cm. By using a photonic sensor, small displacement  $\delta$  can be measured for determining substrate bending quantitatively. Furthermore, as shown on Fig. 4a, we can calculate piezoelectric coefficient  $d_{31}$  through the relationship of  $\delta(E)$ . From Eq. (1), we get the measured  $d_{31}$  of the ZnO thin film, as shown in Fig. 4b, fitted by red curve, in the Fe<sub>3</sub>O<sub>4</sub>/ZnO ME heterostructure is -4.4 pC/N, which is close to theory value of -5.0 pC/N [17, 18].

## 3.3 Microwave ME coupling measurements of Fe<sub>3</sub>O<sub>4</sub>/ZnO heterostructure

Microwave ME interactions and magnetic tunabilities of the Fe<sub>3</sub>O<sub>4</sub>/ZnO multilayer were demonstrated by electrostatic-field-induced in-plane FMR field changes at room temperature, as shown in Fig. 4a. Here, a custom-made microwave FMR spectrometer using a planar transmission line was used to perform the FMR measurements of the ferrite/ferroelectric ME thin films composites at X-band (9.3 GHz). In Fig. 4a, the bias magnetic field, was applied in the Fe<sub>3</sub>O<sub>4</sub>/ZnO film plane with in-plane the microwave RF field and was perpendicular to the DC bias field. A clear electric field induced effective magnetic field 14 Oe, correspondingly, was observed between a bias voltage of -20and 20 V, which is indicated by the electric field induced FMR field change, as shown in bottom right inset of Fig. 4b. Figure 4c shows the FMR field dependence of applied voltage from -30 to 30 V. The FMR field varies linearly as applied voltage switches from -20 to 20 V, indicating the piezoelectric property of ZnO thin film. The FMR field, however, saturates as applied voltage is larger



than 20 V, this result accords with the piezoelectric measurement of ZnO in Fig. 4a, where the displacement of ZnO/glass substrate linearly increases as applied voltage from 0 to 23 V, however, saturated around 23 V. This phenomenon is reasonable because the FMR field won't increase to infinite as applied voltage increase. The Fe<sub>3</sub>O<sub>4</sub>/ZnO heterostructure, can be considered as capacitance, has breakdown voltage limit, which is 23 V in our experiment.

This electric-field-induced FMR field change can be explained by the strain-mediated electrostatic-field-induced magnetic anisotropy field  $H_{eff}$ . The E-field applied across ZnO layer can tune the FMR field of Fe<sub>3</sub>O<sub>4</sub> layer up or down through strain/stress mediated ME coupling [5, 6], see Fig. 4b. The in-plane FMR frequency can be expressed by the well-known Kittel equation [6]:

$$f = \gamma \sqrt{(H_r + H_k + H_{eff})(H_r + H_k + H_{eff} + 4\pi M_s)}$$
 (2)

where  $\gamma$  is the gyromagnetic constant (2.8 MHz/Oe), f is resonance frequency of 9.3 GHz,  $H_r$  is the FMR field,  $H_k$  is the anisotropic field in plane,  $4\pi M_s$  is the magnetization of 5,100 Gauss.  $H_{eff} = 3\lambda_S Y d_{31} E_3 / M_S$  is the E-field induced effective in-plane magnetic field, where, Y is Young's Modulus of Fe<sub>3</sub>O<sub>4</sub> (2.3 × 10<sup>7</sup> N m<sup>-2</sup>),  $\lambda_S$  (28 ppm) is the saturate magnetostriction constant of Fe<sub>3</sub>O<sub>4</sub> at 250 Oe bias magnetic field [24]. In addition, FMR frequency spectrum was measured by applying a voltage on ZnO from -30 to 30 V. We can easily calculate the theoretical  $H_{eff} = 30$  Oe and the corresponding ME coupling coefficient  $\alpha = \Delta H_{eff}$  $\Delta E$  is 3.0  $\times$  10<sup>-4</sup> Oe cm k/V, larger than measured  $H_{eff}$  of 14 Oe and  $\alpha$  of  $1.4 \times 10^{-4}$  Oe cm k/V. The reason is thickness of glass substrate (0.2 mm) is much larger than piezoelectric layer (3 μm), therefore, reduced ME coupling effect due to substrate clamping effect significantly [12, 13].

#### 4 Conclusion

In conclusion, novel magnetic/piezoelectric thin film ME heterostructures of Fe<sub>3</sub>O<sub>4</sub> (1.4 µm)/ZnO (3 µm) on glass substrate were fabricated, which showed a strong ME coupling. A diffusion-free, and well defined interface between iron oxide and zinc oxide layers was achieved due to the low temperature spin spray deposition process. A significant voltage induced in-plane resonance magnetic field shift  $\Delta H_{eff}$  of 14 Oe was observed, corresponding to ME coupling coefficient  $\alpha = \Delta H_{eff}/\Delta E = 1.5 \times 10^{-4}$  Oe cm k/V. Firstly, low temperature spin-spray deposition technology was confirmed as a good synthesis method for depositing thin films ME heterostructures. Secondly, a relative large strain induced FMR frequency shift of 14 Oe was shown in thin film heterostructures compared to other thin films ME structure with ME coupling of 5 6 Oe [12,

13]. This work paved the way for potential multifunctional ZnO-based E-field tuning microwave/RF devices.

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